# $\sigma$ <br> Sigma Journal of Engineering and Natural Sciences Sigma Mühendislik ve Fen Bilimleri Dergisi <br> Research Article <br> IW-PSO APPROACH TO THE INVERSE KINEMATICS PROBLEM SOLUTION OF A 7-DOF SERIAL ROBOT MANIPULATOR 

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#### Abstract

In this paper, two variants of particle swarm optimization (PSO) are used to calculate the inverse kinematics of a new 7 -revolute jointed robot arm. This robot arm is required to move from a position to the desired position with a minimum error in the workspace. A scenario has been set for this purpose. According to this scenario, it is desired that the end effector of the robot arm reach a predetermined position with the minimum error. The results obtained with Random Inertia Weight and Global Local Best Inertia Weight, are compared with the standard PSO. Moreover, the path of the robot arm obtained by cubic trajectory planning is depicted with graphs. Results that computer simulated based, reveal that PSO can be efficiently used for inverse kinematics solution. However, for the inverse kinematic solution, the PSO variables are much more effective than the standard PSO.


Keywords: Inverse kinematics, particle swarm optimization, inertia weight, 7-Dof.

## 1. INTRODUCTION

Especially today, because of the kinematic and dynamic performance, redundant robots (Degree of freedom) attract both industry and researchers. Despite the flexible working structure, the control of these robots is incredibly difficult owing to the large number of joint [1]. The kinematic calculation that is studied in two parts as forward and inverse kinematics, is a scientific discipline that examines robot movements. Forward kinematics that is to determine the position of the end effector from the joint angles, is relatively easy [2]. On the other hand, inverse kinematics that is to obtain the joint angles from the position of the end effector, is a non-linear equations, more complex and impossible to solution by conventional methods such as algebraic, geometric and iterative [3]. Moreover, a redundant robot has infinite number of inverse kinematics solutions. Hence, the most suitable method for this solution is intelligent optimization algorithms such as artificial bee colony, particle swarm optimization, firefly algorithm and artificial neural network [4]. Redundant structure makes impossible to solve with analytical methods, because this robot manipulator has too much the number of joint [5]. This is why researchers have focused on solving the inverse kinematics problem using artificial intelligence algorithms.

[^0]Tejomurtula and Kak used an artificial neural network to perform an inverse kinematic solution of a 3-jointed robot arm. They have achieved a more effective result by eliminating some of the disadvantages such as training time and accuracy, of the BP algorithm [6]. Dash et al. have implemented the inverse kinematic solution of a 6 -articulated robot arm with artificial neural networks [7]. Huang et al. have calculated the inverse kinematic solution of a seven articulated robot manipulator quickly and accurately using classical particle swarm optimization [8]. Ayyıldız and Çetinkaya have designed a new manipulator with 4-DOF and have obtained the inverse kinematic solution of this manipulator with four different intelligent algorithms which are PSO, QPSO, GSA and GA. they demonstrated comparatively results obtained [9]. Rokbani and Alimi have studied the contribution to the of inverse kinematics solution using variants of PSO, such as inertia weight, constriction factor and linear decreasing weight [10]. In addition, they have used a two-jointed robot arm for simulation test. Rokbani et al. have used the firefly method which defined as the newest swarm algorithm, and simulated the results in a three-articulated robot arm [11]. Köker has proposed a new hybrid model consisting of artificial neural network and genetic algorithm for the inverse kinematic solution of a six-axis manipulator [12]. Similarly, Pam et al. have proposed an inverse kinematic solution using bee algorithm and artificial neural network in their work and simulated their work in a three-jointed manipulator. The bee algorithm was used to train the neural network which has a multilayer perceptron structure [13].

The purpose of this work is to perform inverse kinematics calculations of a 7-joint redundant robot arm using the PSO variables which are called Inertia Weight and are very effective in convergence [14], with minimal error and to test the simulation base on a newly designed manipulator.

## 2. KINEMATIC ANALYSIS OF A 7-DOF REDUNDANT ROBOT MANIPULATOR



Figure 1. The structure of 7-DOF robot manipulator
Robotic manipulators which are two ways including prismatic and revolution, consist of links sequentially connected to each other with joints which perform a movement mechanism taking certain angles or by a certain percentage of elongation and shortening by actuators [15]. Designed robot manipulator for this study has 7-DOF with seven revolute joints and is shown in Figure 1. A 7-DOF robotic manipulator not only performs the movement from one position to another position in a comfortably but also has infinite inverse kinematic solutions. Of course, objective is to provide the end effector to be positioned correctly [16]. Today, kinematic calculations are done by homogeneous transformation matrices which are created with the help of four parameters that is called Denavit-Hartenberg parameters [17]. In Table 1, " $i$ " represents the number of joints. The length values are used in meters and the angle values are used in degree. The homogeneous
transformation matrix whi ch is formed by DH parameters in Eq. (1) is used to achieve the robot's kinematic equations [18], [19].

Table 1. DH parameters of 7-Dof redundant manipülatör

| $\mathbf{i}$ | $\mathbf{a i}(\mathbf{m})$ | $\boldsymbol{\alpha i}(\mathbf{D e g})$ | $\mathbf{d i}(\mathbf{m})$ | $\boldsymbol{\Theta i}($ Degree) |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | -90 | $11=0,5$ | $-180<\Theta_{1}<180$ |
| 2 | $12=0,2$ | 90 | 0 | $-90<\Theta_{2}<30$ |
| 3 | $13=0,25$ | -90 | 0 | $-90<\Theta_{3}<120$ |
| 4 | $14=0,3$ | 90 | 0 | $-90<\Theta_{4}<90$ |
| 5 | $15=0,2$ | -90 | 0 | $-90<\Theta_{5}<90$ |
| 6 | $16=0,2$ | 0 | 0 | $-90<\Theta_{6}<90$ |
| 7 | $17=0,1$ | 0 | 0 | $-30<\Theta_{7}<90$ |

${ }_{i-1}^{i} T=\left[\begin{array}{cccc}\cos \theta \mathrm{i} & -\cos \alpha i . \sin \theta \mathrm{i} & \sin \alpha i . \sin \theta \mathrm{i} & \text { ai. } \cos \theta \mathrm{i} \\ \sin \theta \mathrm{i} & \cos \alpha i \cdot \cos \theta \mathrm{i} & -\cos \theta \mathrm{i} \cdot \sin \alpha \mathrm{i} & \text { ai. } \sin \theta \mathrm{i} \\ 0 & \sin \alpha i & \cos \alpha i & d i \\ 0 & 0 & 0 & 1\end{array}\right]$
${ }_{0}^{7} T={ }_{0}^{1} T \cdot{ }_{1}^{2} T \cdot{ }_{2}^{3} T \cdot{ }_{3}^{4} T \cdot{ }_{4}^{5} T \cdot{ }_{5}^{6} T \cdot{ }_{6}^{7} T=\left[\begin{array}{cccc}n_{x} & s_{x} & a_{x} & P_{x} \\ n_{y} & s_{y} & a_{y} & P_{y} \\ n_{z} & s_{z} & a_{z} & P_{z} \\ 0 & 0 & 0 & 1\end{array}\right]$
Where ${ }^{i} \mathrm{~T}_{\mathrm{i}+1}$ is the transfer matrix of link i. ${ }^{0} \mathrm{~T}_{7}$ matrix produces a Cartesian coordinate for any seven joint angles. Because the cost function of the proposed approach is the Euclidian distance in Cartesian space between the obtained and the target points. ${ }^{0} \mathrm{~T}_{7}$ can be used to calculate the Cartesian coordinate of the obtained point in the cost function.

In Eq. (2), Px, Py, and Pz denotes the elements of the position vector whereas nx, ny, nz, sx, $\mathrm{sy}, \mathrm{sz}$, ax, ay, az denote the rotational elements of the transformation matrix [20]. In this study, only the position vector will be used to calculate the position error. The position vector equation is as follows (where s and c represent the sine and cosine functions):

$$
\begin{align*}
& P_{x}=\left(c \theta_{1} c \theta_{2} c \theta_{3} c \theta_{4}-s \theta_{1} s \theta_{3} s \theta_{4}-c \theta_{1} s \theta_{2} s \theta_{4}\right)\left(c \theta_{5} c \theta_{6} l_{7} c \theta_{7}-c \theta_{5} s \theta_{6} l_{7} s \theta_{7}-s \theta_{5} d_{7}+\right. \\
& \left.c \theta_{5} l_{6} c \theta_{6}+l_{5} c \theta_{5}\right)+\left(-c \theta_{1} c \theta_{2} s \theta_{3}-s \theta_{1} c \theta_{3}\right)\left(s \theta_{5} c \theta_{6} l_{6} c \theta_{7}-s \theta_{5} s \theta_{6} l_{7} s \theta_{7}+c \theta_{5} d_{7}+\right. \\
& \left.s \theta_{5} c \theta_{6} l_{6}+l_{5} s \theta_{5}\right)+\left(c \theta_{1} c \theta_{2} c \theta_{3} s \theta_{4}-s \theta_{1} s \theta_{3} s \theta_{4}+c \theta_{1} c \theta_{4} s \theta_{2}\right)\left(-s \theta_{6} l_{7} c \theta_{7}-c \theta_{6} l_{7} s \theta_{7}-\right. \\
& \left.l_{6} s \theta_{6}\right)+c \theta_{1} c \theta_{2}\left(c \theta_{3} c \theta_{4} l_{4}+l_{3} c \theta_{3}\right)-s \theta_{1}\left(s \theta_{3} c \theta_{4} l_{4}+l_{3} s \theta_{3}\right)-c \theta_{1} s \theta_{2} l_{4} s \theta_{4}+c \theta_{1} c \theta_{2} l_{2}  \tag{3}\\
& \left.P_{y}=s \theta_{1} c \theta_{2} c \theta_{3} c \theta_{4}+c \theta_{1} s \theta_{3} c \theta_{4}-s \theta_{1} s \theta_{2} s \theta_{4}\right)\left(c \theta_{5} c \theta_{6} l_{7} c \theta_{7}-c \theta_{5} s \theta_{6} l_{7} s \theta_{7}-s \theta_{5} d_{7}+\right. \\
& \left.c \theta_{5} c \theta_{6} l_{6}+l_{5} c \theta_{5}\right)+\left(-s \theta_{1} c \theta_{2} s \theta_{3}+c \theta_{1} c \theta_{3}\right)\left(s \theta_{5} c \theta_{6} l_{7} c \theta_{7}-s \theta_{5} s \theta_{6} l_{7} s \theta_{7}+c \theta_{5} d_{7}+\right. \\
& \left.s \theta_{5} c \theta_{6} l_{6}+l_{5} s \theta_{5}\right)+\left(s \theta_{1} c \theta_{2} c \theta_{3} s \theta_{4}+c \theta_{1} s \theta_{3} s \theta_{4}+s \theta_{1} s \theta_{2} c \theta_{4}\right)\left(-s \theta_{6} l_{7} c \theta_{7}-c \theta_{6} l_{7} s \theta_{7}-\right. \\
& \left.l_{6} s \theta_{6}\right)+s \theta_{1} c \theta_{2}\left(c \theta_{3} c \theta_{4} l_{4}+l_{3} c \theta_{3}\right)+c \theta_{1}\left(s \theta_{3} c \theta_{4} l_{4}+l_{3} s \theta_{3}\right)-s \theta_{1} s \theta_{2} s \theta_{4} l_{4}+s \theta_{1} c \theta_{2} l_{2}  \tag{4}\\
& P_{z}=\left(-s \theta_{2} c \theta_{3} c \theta_{4}-c \theta_{2} s \theta_{4}\right)\left(c \theta_{5} c \theta_{6} l_{7} c \theta_{7}-c \theta_{5} s \theta_{6} l_{7} s \theta_{7}-s \theta_{5} d_{7}+c+\theta_{5} c \theta_{6} l_{6}+l_{5} c \theta_{5}\right)+ \\
& s \theta_{2} s \theta_{3}\left(s \theta_{5} c \theta_{6} l_{7} c \theta_{7}-s \theta_{5} s \theta_{6} l_{7} s \theta_{7}+c \theta_{5} d_{7}+s \theta_{5} c \theta_{6} l_{6}+s \theta_{5} l_{5}\right)+\left(-s \theta_{6}+\left(-s \theta_{2} c \theta_{3} s \theta_{4}+\right.\right. \\
& \left.c \theta_{2} c \theta_{4}\right)\left(-s l_{7}+\theta_{7}-c \theta_{3} l_{4} s \theta_{4} l_{4}+l_{3} c \theta_{3}\right)-c \theta_{2} s \theta_{4} l_{4}-s \theta_{2} l_{2}+l_{1} \tag{5}
\end{align*}
$$

In the equation (3)(4)(5), if the angle values are known, the position of the end effector can be obtained very easily and this process is referred to as forward kinematics. However, the process of obtaining angle values from position information is called inverse kinematics and it is known as a process that cannot be conducted by conventional methods [21]. In addition, there are infinite inverse kinematics solutions for the 7-DOF robot arm [22]. In this paper, the optimal joint values of the $7-$ DOF robotic manipulator were obtained using particle swarm optimization.

## 3. PARTICLE SWARM OPTIMIZATION AND VARIANTS

### 3.1. Conventional PSO

The particle swam optimization which was developed inspired by a flock of birds, has a powerful search algorithm. Firstly, it is a technique used by Kennedy and Eberhart [23]. This algorithm has some advantages such as its easily applied and having powerful control parameters, compared with other heuristic techniques [24].

The particle swarm optimization is preferred intensively for nonlinear problems which are one of the major problems with the search space and give better solution. In PSO, particles reach optimal solution together using experience and the neighborhood [25].

Only two equations are used to move on the target of particles in PSO, position update equations (Eq. 7) and velocity update equation (Eq. 6). These equations are modified again at each iteration [26].
$v_{i d}=v_{i d}+c_{1} \cdot r_{1} \cdot\left(p_{\text {best }}-x_{i d}\right)+c_{2} \cdot r_{2} \cdot\left(g_{\text {best }}-x_{i d}\right)$
$x_{i d}=x_{i d}+v_{i d}$
Where $\mathrm{d}=1,2, \ldots, \mathrm{D}$ is the dimension and $\mathrm{i}=1,2, \ldots, \mathrm{~S}$ is the swarm size; c 1 and c 2 are weight of personal best and weight of global best, respectively; r1 and r2 are random numbers distributed uniformly in $[0,1]$. The algorithm used in this study is as follows:

- Initialization PSO
- Randomly assign angle values in the appropriate range
- Loop Iteration
- Loop particle
- Perform inverse kinematics calculation (Eq. 3, 4, 5)
- Calculate error value (Eq. 12)
- Find the value of Pbest
- Update particle velocity value
- Update particle angle values
- End Loop Particle
- Compare Gbest with Pbest
- End Iteration
- Return Gbest value


### 3.2. Inertia Weight Strategies in PSO

Sometimes, although the PSO has shown very good convergence in complex problems, it can get stuck near its optimal solution and cannot go any further [27]. Therefore, based on the idea that the PSO algorithm can be developed with some variables, Inertia Weight has been used in many researches and has produced effective results [28]. Inertia weight provides a way to stabilize the particles close to optimal results of search space. So, it has an important role to play in making the correct position of the particle in the search space. It makes this work by contributing to the velocity of the particles [29]. In 1998, Shi and Eberhart have been using inertia weight first time. According to their opinions; although a large inertia weight is very effective in
the global search, a small inertia weight is much more successfully in the local search. In addition, today, some researchers have done studies on the inertia weight dynamically adjustable [30]. Eberhart and Shi [31] have achieved effective results in increasing the velocity of particles at random in each iteration and they call this technique as the random inertia weight (Eq. 8).
$w=0.5+\frac{r a n d 0}{2}$
They have achieved much more effective results increasing the velocity of particles based on global best and local best in each generation. In this way, global-local inertia weight will not have to take both fixed and linearly decreasing values (Eq. 9).
$w=1.1-\frac{g \text { best }}{p b e s t}$
The resulting velocity update equation becomes:
$v_{i d}=w * v_{i d}+c_{1} \cdot r_{1} \cdot\left(p_{\text {best }}-x_{i d}\right)+c_{2} \cdot r_{2} \cdot\left(g_{\text {best }}-x_{i d}\right)$
Inertia weight is used to control the particle velocity. Because, the velocity of particles are a great influence for the convergence of its particles [13]. In this study, the inverse kinematics solution of having redundant feature the 7 -Revolute articulated robot arm was performed with both standard PSO and inertia weight strategies and Results are presented as comparative.

### 3.3. The Method for Solving the Inverse Kinematics Problem

In this study, the aim of the optimization problem is to find the optimum angle value $(\theta)$ for each joint with the given initial Cartesian coordinate and the target coordinate, so the end-effector of robot arm is transferred to desired location by $\theta$. Obviously, the accurate calculations of $\theta$ values are very important.
Error $=\sqrt{\left(x_{2}-x_{1}\right)^{2}+\left(y_{2}-y_{1}\right)^{2}+\left(z_{2}-z_{1}\right)^{2}}$
The main goal of this study is to solve this optimization problem by implementing the PSO. For this purpose, we designed a fitness function that is based on Euclidian distance given equation (12) between the desired location $\left(\mathrm{x}_{2}, \mathrm{y}_{2}, \mathrm{z}_{2}\right)$ and the current location $\left(\mathrm{x}_{1}, \mathrm{y}_{1}, \mathrm{z}_{1}\right)$ described. This cost can be used to calculate fitness function.

## 4. SIMULATION RESULT AND DISCUSSION

The purpose of this paper is to examine how effective and successful of the PSO algorithm to solve the inverse kinematics solution of the 7-Dof serial robot arm. These simulations are performed with the parameters: iteration=5000, particle=300 and each simulation is the best of ten runs between them. The scenario for this study is as follows: The initial position of the manipulator $\left[\theta_{1 i}, \theta_{2 i}, \theta_{3 \mathrm{i}}, \theta_{4 \mathrm{i}}, \theta_{5 \mathrm{i}}, \theta_{6 \mathrm{i}}, \theta_{7 \mathrm{i}}\right]=[0,0,0,0,0,0,0]$, and determined final position (fig. 2) $\left[\theta_{1 f}, \theta_{2 f}, \theta_{3 f}, \theta_{4 f}, \theta_{5 f}, \theta_{f f}, \theta_{7 f}\right]=[45,0,45,0,45,0,0]$.


Figure 2. Final position of the robot arm
Table 2. The results of simulation

| Algorithm | C1 | C2 | Error | Iteratio <br> $\mathbf{n}$ | Time <br> $(\mathbf{s e c})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Conventional PSO | 1,4 | 1,4 | $9,13 \mathrm{e}-03$ | 4773 | 1,9 |
| Random IW | 1,2 | 1,2 | $6,20 \mathrm{e}-03$ | 3789 | 1,6 |
| Global-Local Best IW | 1,2 | 1,2 | $3,64 \mathrm{e}-03$ | 2846 | 1,2 |

A cubic trajectory planning is preferred for locating of the robot arm from initial position to final position. The purpose of this paper is to obtain the joint angles that are optimal values where the end effector is closest to the determined final position, of the end effector of the robot arm. In this study, obtained the results and used the parameters appear in Table 2. According to given results in Table 2, distance between computed position and desired position by global-local best inertia weight smaller than the other two.


Figure 3. Standart PSO position error value (a) and followed by the robot arm trajectory (b)
As shown in Fig. 3a, the error rate of the end effector is reduced by PSO successfully. However, a long road of robot trajectory tracking is possible (Fig. 3b). This reveals the high energy costs. Additional precautions should be taken in the algorithm to avoid this situation. The
evolved optimal solution of joint angle is $\left[\theta_{1 f}, \theta_{2 f}, \theta_{3 f}, \theta_{4 f}, \theta_{5 f}, \theta_{6 f}, \theta_{7 f}\right]=[-180,17.58,-74.28,-11.72,-$ 34.77,11.99, 12.76].


Figure 4. Random inertia weight position error (a) and followed by the robot arm trajectory (b)
In Fig. 4, the results seem to be obtained by the PSO algorithm using Random Inertia Weight strategy. This result is again an optimal result. This result better than standard PSO, but it is a worse result than the Global-Local Best Inertia Weight strategy. The evolved optimal solution is $\left[\theta_{1 f}, \theta_{2 f}, \theta_{3 f}, \theta_{4 f}, \theta_{5 f}, \theta_{f f}, \theta_{7 f}\right]=[102,14.17,-10.07,2.47,24.4,-65.87,-30]$.


Figure 5. Global-local best inertia weight position error and followed by the robot arm trajectory
Fig. 5 represents the best result of this study. This simulation has the best value of the error position and has also come to the fore with the approach results in smaller iterations. According to Fig. $5 b$, the final angle of the joint is as follows $[\theta 1 \mathrm{f}, \theta 2 \mathrm{f}, \theta 3 \mathrm{f}, \theta 4 \mathrm{f}, \theta 5 \mathrm{f}, \theta 6 \mathrm{f}, \theta 7 \mathrm{f}]=$ [62.76,3.45,64.26,20.18,-49.34,-64.68,11.39].

## 5. CONCLUSION

In this paper, inverse kinematics problem have transformed into an optimization problem and this problem is solved with intelligent optimization techniques by a comparative study. The study was carried out as a computer based simulation. The inverse kinematics solutions based on
particle swarm optimization has been performed avoiding time consuming methods and numerical problems. This paper shows that averaged distance by Global-Local Best Inertia PSO smaller than the other two. These simulations clearly indicate that the particle swarm optimization is extremely successful in obtaining the optimal solution of the 7-revolute robotic manipulator. Moreover, the simulation results clearly show that the importance of the inertia weight strategies was highlighted in the article. It can be concluded that contribute to the solution of PSO variable is indisputable.

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